NCAR’S NEW RAMAN-SHIFTED EYE-SAFE AEROSOL LIDAR (REAL)

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ABSTRACT

The design features of, and first observations from, a new eye-safe elastic backscatter lidar system operating at a wavelength of 1.54 \( \mu m \) are presented. Unlike previous lidar transmitters using stimulated Raman scattering in methane, the pump beam is not focused and the cell is injection seeded to improve conversion efficiency and beam quality. The receiver uses custom focusing optics and a 200-\( \mu m \) diameter InGaAs avalanche photodiode (APD). An important achievement was reducing the transmit beam divergence so that it was smaller than the field-of-view (FOV) subtended by the receiver.

The first results were obtained by operating the system in a non-eye-safe dual-wavelength mode (1.064 \( \mu m \) and 1.543 \( \mu m \) simultaneously). Single-wavelength eye-safe operation is achieved by the use of a prism to separate and block the 1.064 \( \mu m \) beam before transmitting into the atmosphere. We are currently developing depolarization ratio measurement capability for use when pointing vertical and a beam steering unit for applications requiring scanning. The system is capable of transmitting over 200 mJ/pulse at 10 Hz at 1.543 \( \mu m \). Examples of backscatter data from vertical and horizontal pointing periods are shown.

1. MOTIVATION

Since January of 2002, NCAR’s Atmospheric Technology Division has been developing an eye-safe aerosol backscatter lidar at 1.54 \( \mu m \) wavelength. The original goal of the project was to produce a completely eye-safe aerosol backscatter lidar that could be deployed in atmospheric research field campaigns to monitor vertical profiles of aerosol backscatter in the lower troposphere. We have far surpassed our original goal by producing sufficient power to see aerosol structures at 10 km range when pointed almost horizontally. This success has inspired us to move towards scanning and depolarization ratio measurement capabilities. We expect to complete our first field demonstrations in a mobile seatainer during the spring and summer of 2004. A more complete description of the transmitter and receiver can be found in Mayor et al.[1]

2. TRANSMITTER

The lidar transmitter begins with a flash-lamp pumped, Q-switched, Nd:YAG laser capable of generating 800 mJ/pulse energy at 1.064 \( \mu m \) wavelength. The pump beam is converted to the eye-safe wavelength via stimulated Raman scattering (SRS) in a high pressure cell filled with pure CH\(_4\). SRS is a third-order, nonlinear, inelastic scattering process whereby a sufficiently-high pump field excites molecular vibrations in a medium. The frequency of the scattered light (Stokes output) is shifted by the frequency of these vibrations. The Stokes field is initiated by the spontaneous emission of a photon and therefore the energy and spatial characteristics will fluctuate. To
avoid these fluctuations one can seed the cell with a stable tunable Stokes wavelength laser. We injection seed our Raman cell with a continuous-wave 20 mW telecom diode laser which is coupled to a single mode fiber which emits a near perfect Gaussian beam.

The Raman cell was custom built and improved from the design of Kurnit et al.[3]. The internal mirrors have a high reflectivity coating at 1.064 µm and 1.540 µm and high transmission at the second Stokes line (2.8 µm) and the first anti-Stokes line (0.81 µm) to suppress build-up at these wavelengths. It is important to note, however, that the pump beam is not focused in the cell. Focusing a high energy beam in methane, often causes optical breakdown and leaves carbon/soot deposits on mirrors and windows—limiting long term operation of the transmitter.[4; 5] Internal fans circulate the methane. A diagram of the experimental setup is shown in Fig. 2.

### 3. RECEIVER

For the results presented here, our lidar receiver used a commercially available 40 cm diameter f/10 Schmidt-Cassegrain telescope. The telescope is mounted in a fixed vertical position on an optics table. The backscatter light collected by the telescope is collimated with a doublet lens to facilitate transmission through subsequent interference filters. The lens is followed by a short-wave-pass dichroic to separate 1.064 µm and 1.543 µm backscatter. Both wavelengths are filtered by a narrow band pass interference filter to reject background light. The 1.064 µm light passing through it’s filter is focused, via a single element aspheric lens, onto a 1.5 mm diameter active area, long wavelength enhanced, silicon APD. A custom focusing lens was designed to focus the eye-safe backscatter onto a photodiode. The lens is a three element design, a doublet with companion meniscus lens, with a 18 mm focal length and 12.4 mm diameter. The lens was designed to collect all light within a 0.50 mrad full-angle onto the detector for the range 500 m to 15 km. In practice, the useful range of the instrument is slightly adjustable—analogous to the depth-of-field of a camera. The photodetector is a 200 µm diameter InGaAs/InP APD with 75% quantum efficiency and a bandwidth of 200 MHz.

Backscattered photons are converted to electrons by the photodetectors and the resulting electrical signals are amplified and digitized. For the 1.064 µm channel, the detector package uses a 10 MHz bandwidth linear transimpedance amplifier. Prior to the this time of this writing, the 1.543 µm signal is amplified by a operational amplifier that has a bandwidth of 55 MHz at a gain of 20. In order to amplify return signals that are near the noise level of the detector we operate the with a gain of approximately 850 which reduces the bandwidth to approximately 1 MHz. We are currently in the process of replacing that detector and amplifier with a Perkin Elmer C30659-1500-R2A InGaAs APD/preamplifier combination module with 50 MHz bandwidth.

Several factors can limit the range resolving capability of a backscatter lidar system. The 1.543 µm pulse duration is 4 ns which corresponds to 1.2 m in space. The InGaAs APD has a bandwidth of 200 MHz with an equivalent rise time of 1.8 ns which corresponds to approximately 30 cm in range. However, as stated earlier, the bandwidth of our present amplifier is 1 MHz with an equivalent rise time of 350 ns which corresponds to approximately 53 m in range. The digitizer sampling rate controls the spacing of the data points despite they may not be independent samples due to one of the slower previous components. Our digitizer is capable of 100 MSPS in single-channel mode, however we typically use it in a 50 MSPS dual-channel mode. 50 MSPS is equivalent to 3 m spatial sampling. We expect the new Perkin Elmer C30659-1500-R2A to improve our range resolution to about 3 m.
4. DEPOLARIZATION

The ability to discern liquid water droplets from ice crystals is useful in studies of clouds and well documented[6]. We are in the process of adding this capability to REAL. In order to do it, we first had to improve the polarization purity of our pump laser by passing the light through a thin film plate resulting in a 200:1 polarization ratio which is improved from 70%. Unfortunately, we loose about 150 mJ/pulse of the pump. This in turn reduces the total transmit power at 1.54 µm to approximately 170 mJ/pulse.

In the receiver we use a custom calcite polarization beam-splitter cube to separate the orthogonal polarization states. The cube is 25.5 mm clear aperture and results in 200,000:1 separation ratio. We will use two identical detector systems to measure the depolarization ratio at 50 MHz per channel.

5. BEAM STEERING UNIT

At the time of this writing, a beam steering unit (BSU) was being constructed for the lidar system. The BSU features a 17” clear aperture and capability to make full azimuth and elevation scans. The horizontal collar of the BSU contains a 16 channel slip-ring to transmit power to and exchange data with the elevation drive. This features allows continuous PPI type scans in one direction. Computer controlled motors (Animatic) with angle encoding allow full control and feedback of the mirror positions.

A ray-trace analysis of the receiver indicates that each BSU mirror must be flat to within 3 waves (0.9 µm of sag) across the full aperture. This flatness tolerance is relaxed compared to most optical surfaces, but sufficient because lidar systems are non-imaging. The flatness requirement was driven mainly by the detector diameter, and to a lesser degree the other optics in the receiver sub-system. We have chosen Zerodur as the substrate material and protected gold-coatings for wavelength flexibility and high reflectivity in the 1.5 µm region.

6. RESULTS AND DISCUSSION

The highest Stokes energy was obtained with a 3.4 m interaction length at a pressure of approximately 10 atm. In this configuration, 1.543 µm energies in excess of 250 mJ/pulse were measured corresponding to better than 45% photon conversion efficiency. A significant enhancement of Stokes conversion efficiency, particularly at lower pressures, was seen with injection seeding and beam M^2 was improved from ∼16 to ∼11. The improvement in beam quality factor was critical for full overlap with our receiver system.

When collecting data with the 1.064 µm wavelength from our laboratory, we use a vertically pointed 3-cm wavelength Doppler radar for safety.[7] The radar provides a cone of microwave radiation surrounding the transmit beam. Software algorithms that identify aircraft echoes in the radar return turn off the laser immediately if an aircraft is detected.

In the data shown here, we have averaged together backscatter from consecutive groups of 10 laser shots to form 1 s averages. The backscatter signals were sampled at 50 MHz to provide data points at 3 m intervals in range. The DC baseline of each average return, which is proportional to the background intensity, is subtracted based on an average of data points sampled before the laser is fired. The average lidar return is then corrected for one-over-range-squared dependence. Figure 4 shows the backscatter intensity for the 1.543 µm and 1.064 µm wavelengths collected simultaneously when the beam was pointed vertically. Both images in Fig. 4 show the detailed vertical structure of the entrainment zone of a convective boundary layer. A visual comparison of the time-versus height images indicate the 1.54 µm data are smoother. We attribute this to the bandwidth difference of the amplifiers of the two channels. Despite this difference, the comparison shows excellent agreement and demonstrates the ability to resolve fine scale detail at the eye-safe wavelength.

An important achievement was the ability to generate high energy pulses with good spatial quality. The receive FOV was severely restricted by the small diameter detector that we used. Therefore, steps were taken to minimize transmit beam divergence, maximize the receive FOV, and minimize the range of achieving full overlap. These included (1) coaxial transmit beam and receive FOV; (2)
injection seeding of Raman cell; (3) transmit beam expander; and (4) custom focusing optics in front of the detector.

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REFERENCES